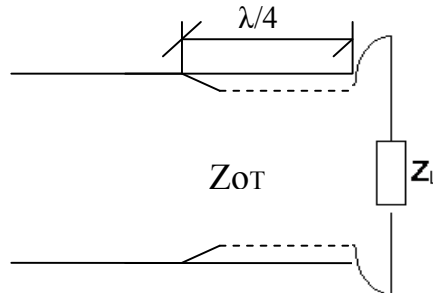


### Matching Networks Problems:

1. In order to match a 300-Ω load to a 75- Ω transmission line, a quarter-wave transformer is used. Find the characteristic impedance of  $\lambda/4$  x'former.

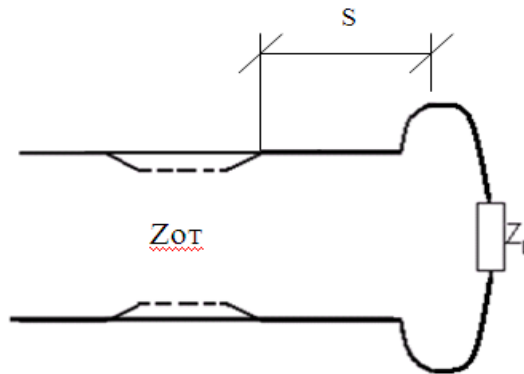
Solution:



$$Z_O = \frac{Z_{OT}^2}{R_L}; Z_{OT} = \sqrt{Z_O R_L} = \sqrt{75(300)} = 150 \Omega$$

2. An antenna has a feedpoint of  $Z_L = (100 - j80) \Omega$ . The characteristic impedance of this antenna is 75 Ω. Determine (a) the shortest distance from the load which a  $\lambda/4$  x'former may be inserted to provide matching; (b)  $Z_{OT}$ .

Solution:



$$\Gamma = \frac{Z_L - Z_O}{Z_L + Z_O} = \frac{100 - j80 - 75}{100 - j80 + 75} = 0.436 \angle -48.08^\circ$$

$$SWR = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.436}{1 - 0.436} = 2.55$$

$$S_{\max} = \frac{\phi}{2\beta} = \frac{-48.08^\circ}{2\left(\frac{360^\circ}{\lambda}\right)} = -0.0667\lambda; \text{ make } \lambda \text{ positive: } -0.0667\lambda + 0.5\lambda = 0.433\lambda$$

$$S_{\min} = \frac{\phi + 180^\circ}{2\beta} = \frac{-48.08^\circ + 180^\circ}{2\left(\frac{360^\circ}{\lambda}\right)} = 0.183\lambda$$

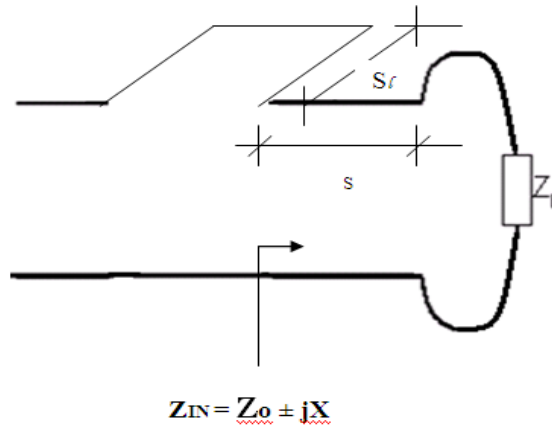
Since  $S_{\min}$  is closer to the load, choose  $S_{\min} = 0.183\lambda$ .

(b) Since load is resistive:  $R_{\min} = \frac{Z_0}{\text{SWR}} = \frac{75}{2.55} = 29.41\Omega$

$$Z_{OT} = \sqrt{Z_0 R_L} = \sqrt{75(29.41)} = 46.97\Omega$$

3. For a TL with  $Z_0 = 50\Omega$  and a load impedance of  $Z_L = (120 + j100)\Omega$ , determine the distance where a series stub must be placed from the load to the line and determine the length of the stub.

Solution:



$$Z_{in} = Z_0 \pm jX = 50 \pm jX$$

$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan \beta S}{Z_0 + jZ_L \tan \beta S}; \text{ let } A = \tan \beta S$$

$$50 \pm jX = 50 \frac{120 + j100 + j50A}{50 + j(120 + j100)A}$$

$$50 \pm jX = 50 \frac{120 + j100 + j50A}{50 + j(120 + j100)A}$$

$$50 \pm jX = 50 \frac{120 + j(100 + 50A)}{(50 - 100A) + j120A} \cdot \frac{(50 - 100A) - j120A}{(50 - 100A) - j120A}$$

$$50 \pm jX = 50 \frac{120(50 - 100A) + (100 + 50A)(120A) + j(100 + 50A)(50 - 100A) - j120(120A)}{(50 - 100A)^2 + 120^2 A^2}$$

Equate real parts:

$$50 = 50 \frac{6000 - 12000A + 12000A + 6000A^2}{2500 - 10000A + 10000A^2 + 14400A^2}$$

$$2500 - 10000A + 10000A^2 + 14400A^2 = 6000 - 12000A + 12000A + 6000A^2$$

$$18400A^2 - 10000A - 3500 = 0$$

Solve for the roots:  $A_1 = 0.78561$ ;  $A_2 = -0.24213$

$$0.78561 = \tan\left(\frac{360^\circ}{\lambda}\right)S_1 ; S_1 = 0.106\lambda$$

$$-0.24213 = \tan\left(\frac{360^\circ}{\lambda}\right)S_2 ; S_2 = -0.0378\lambda \text{ or } -0.0378\lambda + 0.5\lambda = 0.4622\lambda$$

Since  $S_1$  is closer to the load, insert the stub at a distance  $0.106\lambda$  from the load.

$$Z_{in} = 50 \frac{120 + j100 + j50(0.78561)}{50 + j(120 + j100)(0.78561)} = 50 - j78.79$$

The series stub must have an input impedance of  $Z_{ins} = j78.79\Omega$  to tune out the  $-j78.79\Omega$  reactance.

For the length of the stub:

a) Short circuit stub

$$Z_{ins} = jZ_0 \tan \beta S_l ; j78.79 = j50 \tan \beta S_l$$

$$\tan \beta S_l = 1.5758 ; \left(\frac{360^\circ}{\lambda}\right)S_l = 57.6^\circ$$

$$S_l = 0.16\lambda$$

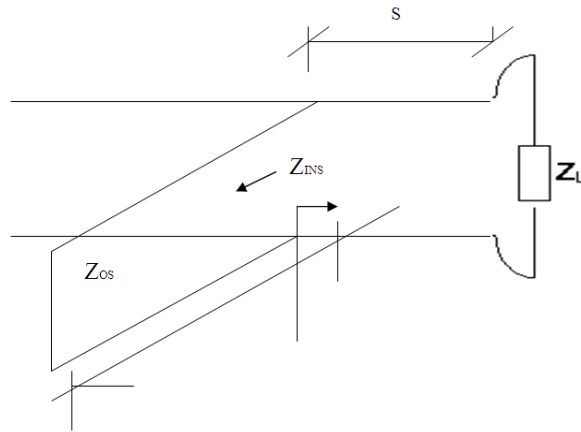
b) Open circuit stub

$$Z_{ins} = -jZ_O \cot \beta S_l; j78.79 = -j50 / \tan \beta S_l$$

$$\tan \beta S_l = -0.6346; \left(\frac{360^\circ}{\lambda}\right) S_l = -32.4^\circ$$

$$S_l = -0.09\lambda; \text{making } \lambda \text{ positive } : 0.41\lambda$$

4. A series RC combination having  $Z_L = (120 - j100) \Omega$  at 10 MHz is connected to a 75  $\Omega$  transmission line. Calculate the position and the length of a shunt stub that will match the load to the line.



$$Y_{in} = G \pm jB = 1 / Z_{in}$$

$$Y_{in} = \frac{1}{Z_O \frac{Z_L + jZ_O \tan \beta S}{Z_O + jZ_L \tan \beta S}}; \text{let } A = \tan \beta S$$

$$\frac{1}{75} \pm jB = \left(\frac{1}{75}\right) \frac{Z_O + jZ_L A}{Z_L + jZ_O A}$$

$$\frac{1}{75} \pm jB = \left(\frac{1}{75}\right) \frac{75 + j(120 - j100)A}{(120 - j100) + j75A}$$

$$\frac{1}{75} \pm jB = \left(\frac{1}{75}\right) \frac{(75 + 100A) + j120A}{120 + j(75A - 100)} \cdot \frac{120 - j(75A - 100)}{120 - j(75A - 100)}$$

$$\frac{1}{75} \pm jB = \left(\frac{1}{75}\right) \frac{(75 + 100A)(120) + 120A(75A - 100) + j(120A)(120) - j(75 + 100A)(75A - 100)}{120^2 + (75A - 100)^2}$$

Equate real terms:

$$\frac{1}{75} = \left(\frac{1}{75}\right) \frac{(75 + 100A)(120) + 120A(75A - 100)}{120^2 + (75A - 100)^2}$$

$$120^2 + (75A - 100)^2 = (75 + 100A)(120) + 120A(75A - 100)$$

$$144000 + 5625A^2 - 15000A + 10000 = 9000 + 12000A + 9000A^2 - 12000A$$

$$3375A^2 + 15000A - 15400 = 0$$

Solve for the roots:  $A_1=0.8602$ ;  $A_2=-5.305$

$$0.8602 = \tan\left(\frac{360^\circ}{\lambda}\right)S_1 ; S_1 = 0.1131\lambda$$

$$-5.305 = \tan\left(\frac{360^\circ}{\lambda}\right)S_2 ; S_2 = -0.2203\lambda \text{ or } -0.2203\lambda + 0.5\lambda = 0.2797\lambda$$

Since  $S_1$  is closer to the load, insert the stub at a distance  $0.1131\lambda$  from the load.

$$Y_{in} = \left(\frac{1}{75}\right) \frac{75 + j(120 - j100)(0.8602)}{(120 - j100) + j75(0.8602)} = (0.0133336 + j0.01541)S$$

The shunt stub must have an input admittance of  $Y_{ins} = -j0.01541S$  to tune out the  $j0.01541 S$  susceptance.

For the length of the stub:

a) Short circuit stub:

$$Y_{ins} = \frac{1}{Z_{ins}} = \frac{1}{jZ_0 \tan \beta S_l} ; -j0.01541 = \frac{1}{j75 \tan \beta S_l}$$

$$\tan \beta S_l = 0.86524 ; \left(\frac{360^\circ}{\lambda}\right)S_l = 40.8676^\circ$$

$$S_l = 0.1135\lambda$$

b) Open circuit stub

$$Y_{ins} = \frac{1}{Z_{ins}} = \frac{1}{-jZ_0 \cot \beta S_l} ; -j0.01541 = \frac{\tan \beta S_l}{-j75}$$

$$\tan \beta S_l = -1.15575 ; \left(\frac{360^\circ}{\lambda}\right)S_l = -49.1324^\circ$$

$$S_l = -0.1365\lambda + 0.5\lambda = 0.3635\lambda$$